

A NEW METHOD FOR PREDICTING
PERFORATION ENTRANCE HOLE DIAMETER

IPS 16-37

GEODynamics®

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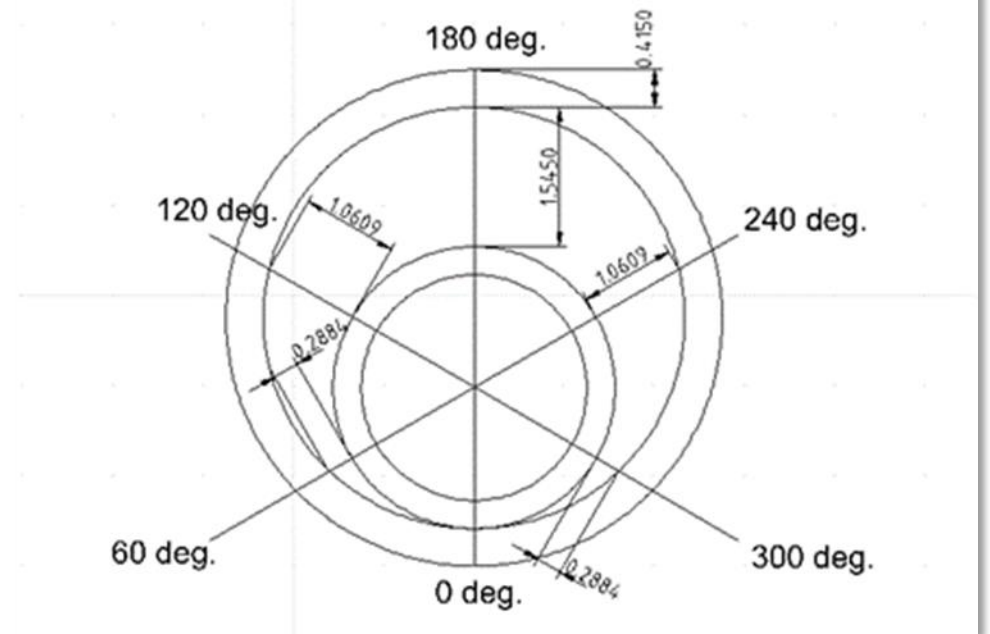
INTRODUCTION

- An accurate measurement of perforation entrance hole diameter is important when planning and executing a hydraulic fracturing operation
- Entrance hole diameter variability with phasing must be known when:
 - Selecting the proppant diameter in order to reduce bridging;
 - Estimating perforation friction, especially in limited entry applications; and
 - Using ball sealers.
- Various charges shot at a number of clearances in order to develop EHD correlation
- API 19B Section 1 data (or equivalent) used – with the forthcoming Section 7 testing the method can be further refined

ENTRANCE HOLE VARIATION WITH CLEARANCE

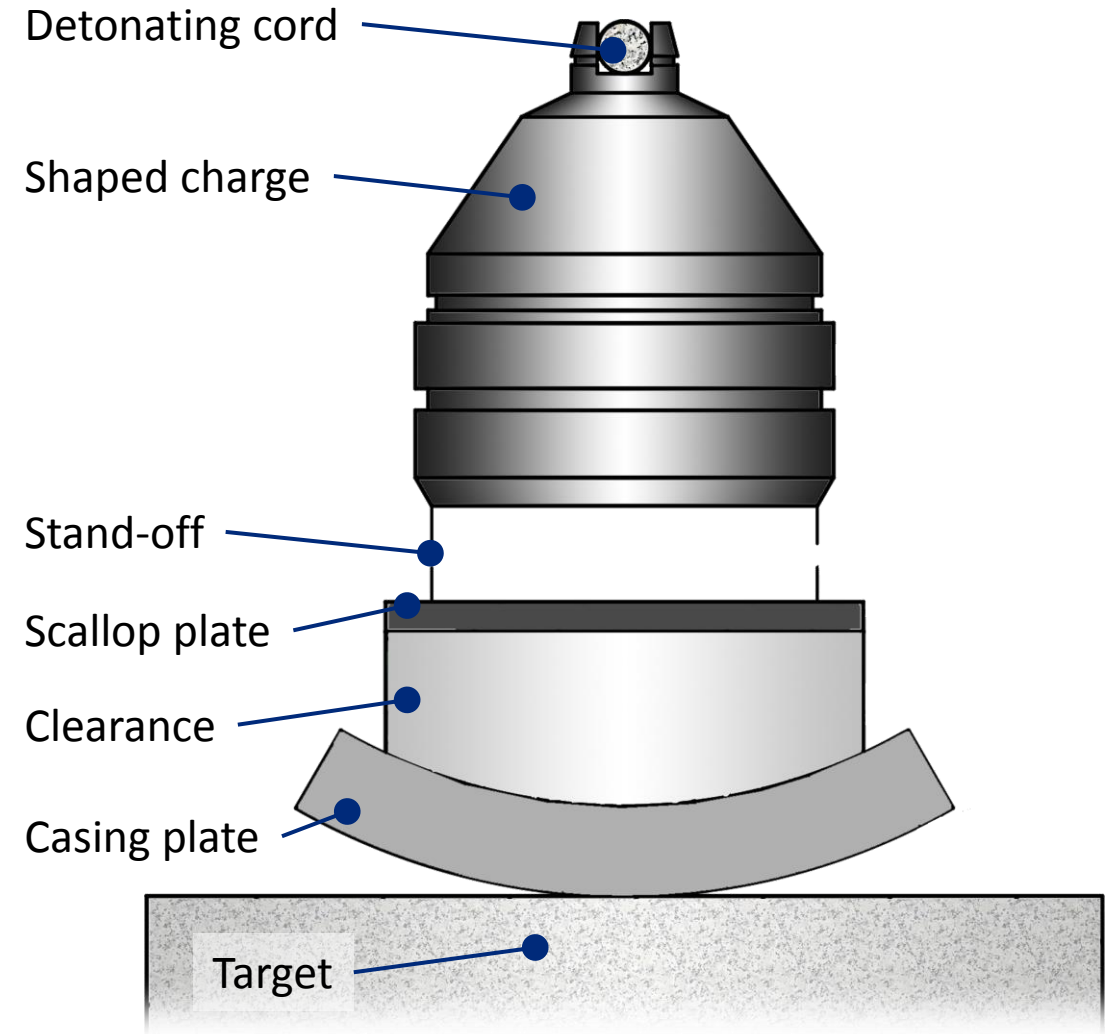
- In a decentralized configuration the clearance varies around the circumference and as a result the entrance hole diameter varies (sometimes significantly)
- The variation is recorded in the API 19B Section 1 test and the resulting data can be used in situations where the same configuration will be used in a well
- But what about the situation where the same charge and carrier will be shot in a different sized casing?

3.125 inch Gun decentralized inside 5.5 in 23# Casing



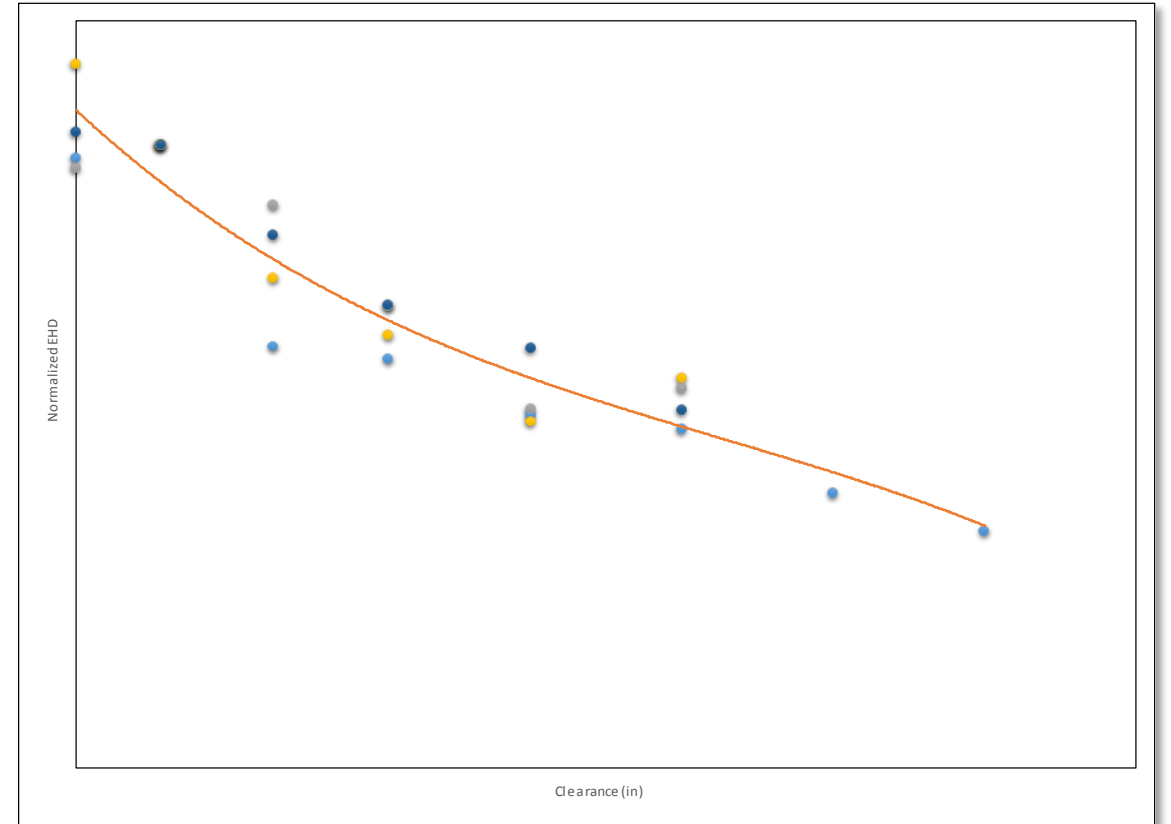
TEST CONFIGURATION

- Selection of charges shot in a test jig - all under the same configuration and casing dimension
- Jig simulated charge stand-off, scallop, clearance, and casing
- Used a segment of casing rather than flat plate
- Each charge shot at clearances ranging from 0 – 3 inches



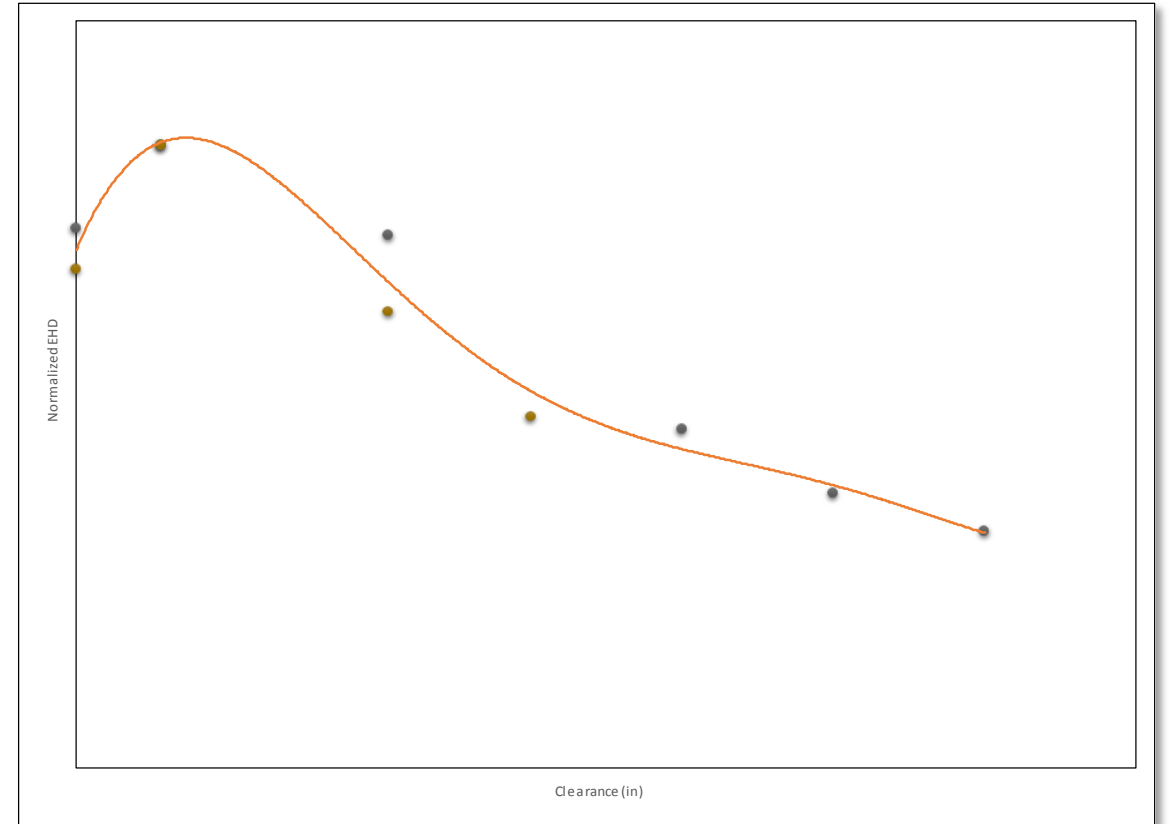
ANALYSIS

- Analysis of the data resulted in the development of a number of “type” curves
- Certain charges exhibit similar variations in EHD with clearance



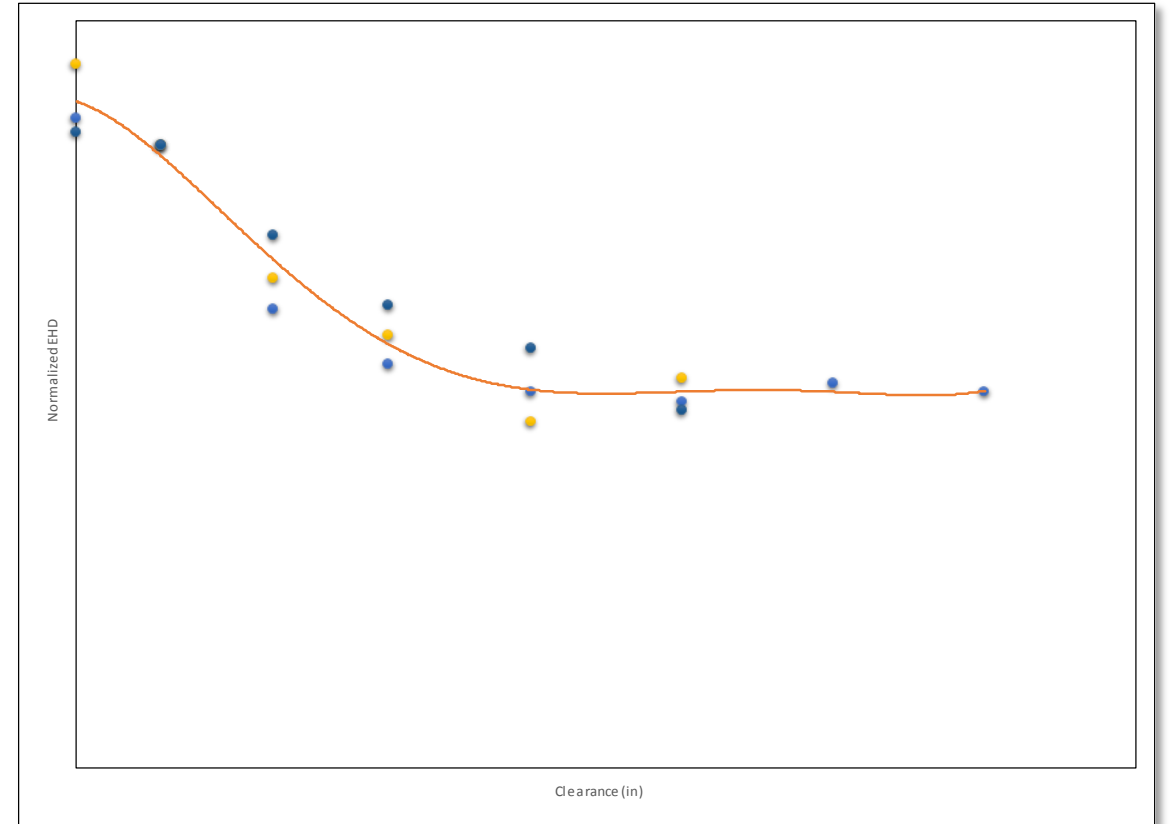
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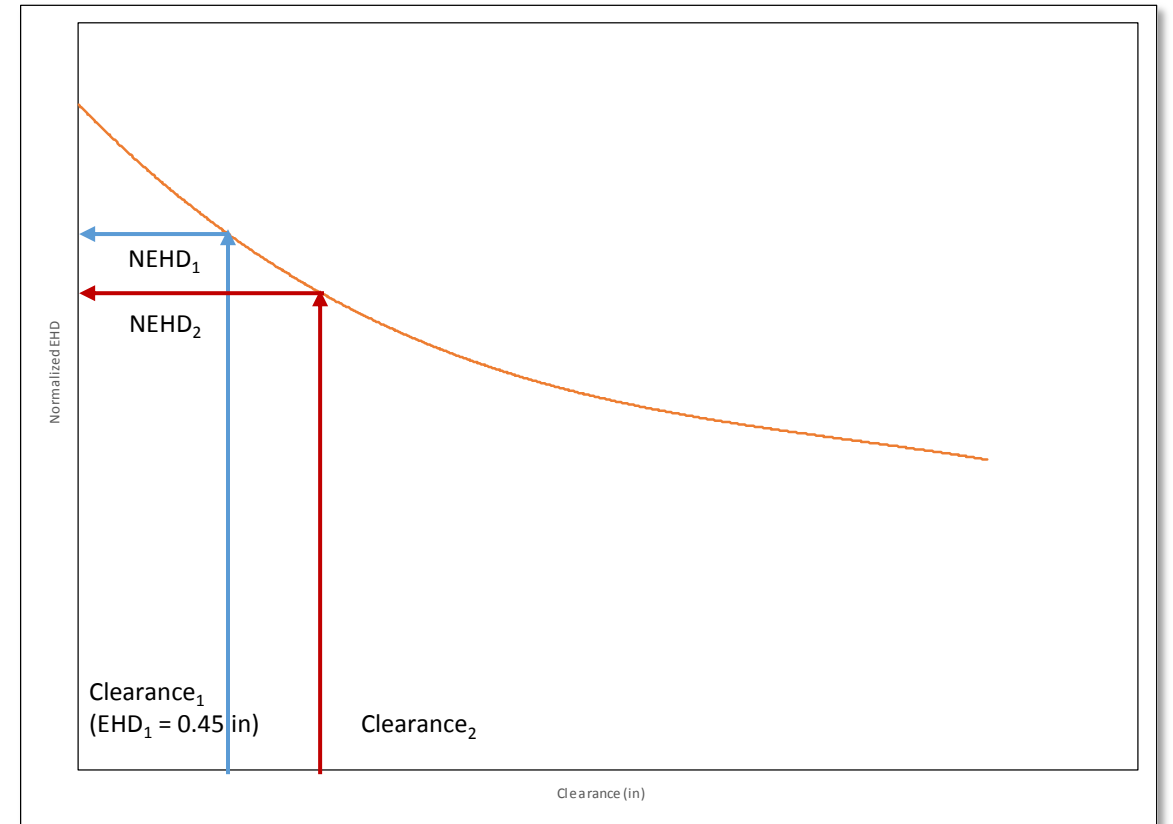
APPLYING THE CORRELATION

- Optimally need data for a specific charge at a few clearances as is available on an API RP19B, API RP43F, or from a QC datasheet
- Determine which correlation is applicable by testing the charge data against correlations
 - Use the correlation resulting in the least amount of error/deviation

API FORM 43F		CERTIFICATION DATA SHEET		PERFORATING SYSTEM EVALUATION, RP 43, SECTIONS 1 AND 2		3-3/8" EXPENDABLE, 6 SPF 60°					
Service Company		Explosive Weight	23 gm	HMX powder, Case Material	STEEL						
Gun OD & Trade Name	3-3/8" EXPENDABLE, 6 SPF 60°	Max. Temp. F	400	1 hr	3 hr	24 hr	100 hr				
Charge Name		Maximum Pressure Rating	22,700	psi, Carrier Material	STEEL						
Manufacturer Charge Part No.		Date of Manufacture	5/4/2007	Shot Density	6	shots/ft					
Gun Type	SCALLOPED GUN (RETRIEVABLE, EXPENDABLE HOLLOW STEEL CARRIER)	Recommended Minimum ID for Running	3.8	in.							
Phasing Tested	60 degrees, Firing Order	X	Top down,	X	Bottom up	Available Firing Mode	X				
Debris Description	SMALL STEEL PARTICLES MAY EXIT CARRIER	Debris Weight	N/A	gm/charge, Debris	N/A	Simultaneous.	X				
Remarks	GUNS MAY BE TUBING OR WIRELINE CONVEYED										
SECTION 1 - CONCRETE TARGET											
Casing Data	4-1/2"	OD, Weight	11.6	lb/ft,	L-80	API Grade, Date of Concrete Test	6/22/2007				
Target Data	120	OD, Briquet Compressive Strength	7152	psi, Age of Target		28	days				
Shot No.	No. 1	No. 2	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No. 10	
Clearance, in.	0.00	0.14	0.45	0.63	0.45	0.14	0.00	0.14	0.45	0.63	
Casing Hole Diameter, Short Axis, in.	0.47	0.45	0.44	0.42	0.43	0.44	0.47	0.45	0.44	0.42	
Casing Hole Diameter, Long Axis, in.	0.47	0.46	0.44	0.42	0.44	0.45	0.48	0.45	0.45	0.43	
Average Casing Hole Diameter, in.	0.47	0.46	0.44	0.42	0.44	0.45	0.48	0.45	0.45	0.43	
Total Depth, in.	47.50	46.20	45.40	44.20	46.90	48.30	49.20	48.10	42.50	47.10	
Burr Height, in.	0.04	0.04	0.05	0.05	0.07	0.04	0.04	0.06	0.04	0.05	
Shot No.	No. 11	No. 12	No. 13	No. 14	No. 15	No. 16	No. 17	No. 18	No. 19	No. 20	Average
Clearance, in.	0.45	0.14									0.30
Casing Hole Diameter, Short Axis, in.	0.42	0.46									0.44
Casing Hole Diameter, Long Axis, in.	0.43	0.46									0.45
Average Casing Hole Diameter, in.	0.43	0.46									0.45
Total Depth, in.	46.30	44.10									46.32
Burr Height, in.	0.05	0.04									0.05
Remarks	PENETRATION NORMALIZED TO 5000 PSI CONCRETE WOULD BE 51.30" (5% PER 1,000 PSI)										
SECTION 2 - BEREA SANDSTONE CORE TARGET											
	Shot No.	No. 1	No. 2	No. 3	No. 4	No. 5	No. 6	Average			
Berea Bulk Porosity,	Faceplate Hole Diameter, Short Axis, in.										
	Faceplate Hole Diameter, Long Axis, in.										
Date of Berea Test	Average Faceplate Hole Diameter, in.										
	Total Depth, in.										
CERTIFICATION											
Type of Certification:	<input checked="" type="checkbox"/> Self <input type="checkbox"/> Third Party										
I certify that these tests were made according to the procedures as outlined in API RP 43: Recommended Practices for Evaluation of Well Perforators, Fifth Edition, January 1991. All of the equipment used in these tests, such as the guns, jet charges, detonator cord, etc., was standard with our company for use in the gun being tested, and was not changed in any manner for the test. Furthermore, the equipment was chosen at random from stock and therefore will be substantially the same as the equipment which would be furnished to perforate a well for any operator.											
CERTIFIED BY		(Company Officer)		(Title)		(Date)		(Company)			(Address)
RECERTIFIED											
<input checked="" type="checkbox"/> PRELIMINARY											

APPLYING THE CORRELATION

- For a given clearance (Clearance_1) on the datasheet determine the corresponding value for the Normalized EHD (NEHD_1)
- From the data sheet also record the corresponding EHD (EHD_1) for Clearance_1
- Determine the Normalized EHD (NEHD_2) for the clearance (Clearance_2) to be determined
- Use ... $\text{EHD}_2 = \text{EHD}_1 * \text{NEHD}_2 / \text{NEHD}_1$
- A similar correlation has been developed for SBH charges



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QUESTIONS? THANK YOU!

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